IN THE SPECIFICATION

Please delete the heading at page 10, line 13 and the following paragraph beginning at page 10, line 14.

Please amend the heading at page 10, line 19 as follows:

Example [[8]] 7: (inventive)

Please amend the heading at page 10, line 26 as follows:

Example [[9]] 8: (inventive)

Please amend the heading at page 10, line 31 as follows:

Example [[10]] 9: (inventive)

Please amend Table 1 beginning at page 11, line 5 as follows:

| Example | Modulus of elasticity [-] | Tensile strength [N/mm$^2$] | Tensile strength at break [%] |
|---|---|---|---|
| 4 | 1674 | 47.5 | 22.7 |
| 5 | 1955 | 47.6 | 6.7 |
| 6 | 1805 | 49.1 | 17.9 |
| ~~7~~ | ~~1697~~ | ~~46.6~~ | ~~26.8~~ |
| [[8]] 7 | 3337 | 46.4 | 3.4 |
| [[9]] 8 | 1912 | 47.5 | 9.0 |
| [[10]] 9 | 1885 | 48.0 | 19.3 |

Please amend the paragraph beginning at page 11, line 7 as follows:

From the examples it can be seen very clearly that the moldings of the invention made from sintering powder of the invention as in Examples ~~2 to 6~~ 5 to 9 have markedly higher modulus of elasticity than moldings made from conventional sintering powder. The tensile strength of the moldings of the invention is little different, if at all, from the tensile strength of the molding made from conventional sintering powder. The tensile strain at break shows that moldings of the invention have markedly lower tensile strain at break. Since a higher modulus of elasticity results in lower flexibility and low tensile strain at break, the powder of the invention can therefore be laser-sintered to produce prototype components which have to have high dimensional stability, e.g. gearwheels.